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Multi-criteria Approach and Wind Farm Site Selection Analysis for Improving Power Efficiency

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Abstract

The use of electrical energy is still increasing around the world and is extending to cover more electrical power-based applications. This will lead to more climate change across the globe in the next decades. Thus, renewable energy must be used in an efficient way to reduce the negative effects of these power generators. The location of the wind farm plays a big role in determining the efficiency of the output power. The aim of this research is to study which turbine configuration suits best for a specific location, taking into consideration all the possible constraints. In order to reach our goal, three different turbine configurations are studied with the least possible uncertainties. The optimal configuration is when the wind shear is minimal at the height of the hub, the wake effect is negligible, and the capacity factor is maximal (the economical part is not included). In this study, the Sorochi Gory (located in Tatarstan, Russia) wind farm site will be explained and analysed. The power exponent and capacity factor will be calculated, and the results will be displayed.

Keywords: Wind Farm; Wind Shear; Turbines Configuration; Capacity Factor.

1. Introduction

Wind farm location is an important factor to be studied before building turbines to get the highest power efficiency. Sorochi Gory is a location where wind turbines will be built; a mast will be placed on the site to measure the wind speed from July 2018 to July 2019 in order to estimate the energy output. In this paper, the power curves are studied, panoramic views in all directions are shown to reflect the shear length, the area will be analysed and information about it will be presented [1, 2]. Due to confidentiality, some of the values are not shown; however, the calculation procedure and results are presented. The project is intended to produce 150 MW using 60 wind turbines. The three types of turbines are Siemens Gamesa SG 3.4-132 3.465MW, Vestas V126-3.45 MW HTq and Lagerwey L100-2.5 MW.

1.1. Site Location

A site is carefully chosen to be suitable to build a wind farm on; primarily, the area should be rural away from any human activity to avoid noise damage and no tall buildings to avoid turbulence. Nearby electric stations are an advantage to connect the wind farm to the grid. The Sorochi Gory project is located approximately 65 km southeast of the city of Kazan in the republic of Tatarstan. Figure 1 shows the boundary of the wind farm area.

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Figure 1. Map of Sorochi Gory wind farm site

It is worth noting that from the south it is bounded by the Kama River. The river delivers low turbulence [3].

1.2. Wind Speed on the Site

Figure 2 shows the approximate mean wind speed in Sorochi Gory and the cities around it according to Atlas [4].

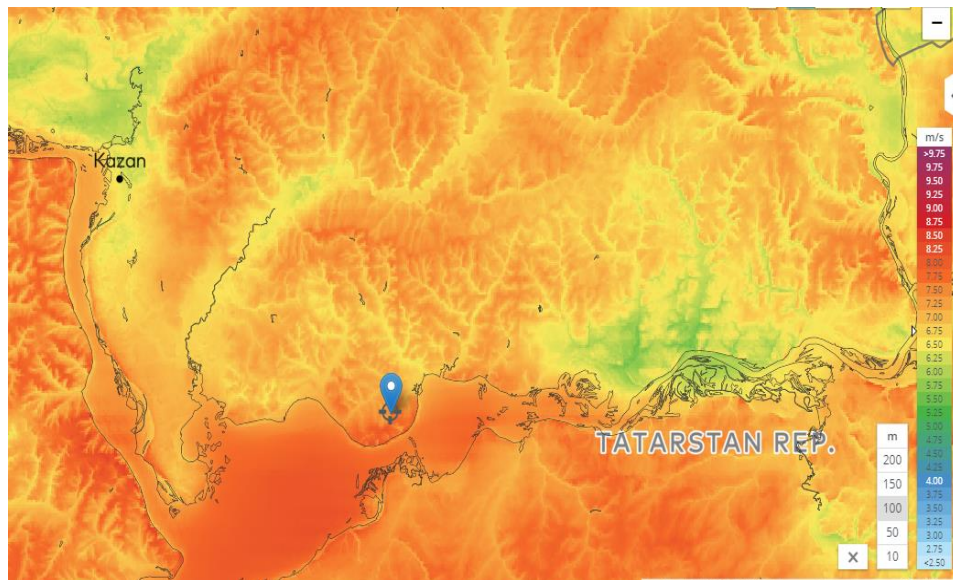


Figure 2. Map presenting the mean wind speed around Tatarstan

As seen in the Figure 2, the wind speed is considerably intense in the referred area with respect to other areas within its boundaries. The area below Sorochi Gory is the Kama River, more studies can be made for an offshore wind farm construction [5]. Figure 3, showing the mean wind speed in Sorochi Gory.

As seen from the Figure 3, the wind speed across the site is between 7.25 and 8 m/s, which makes it suitable to be categorised in the class 2 according to IEC.

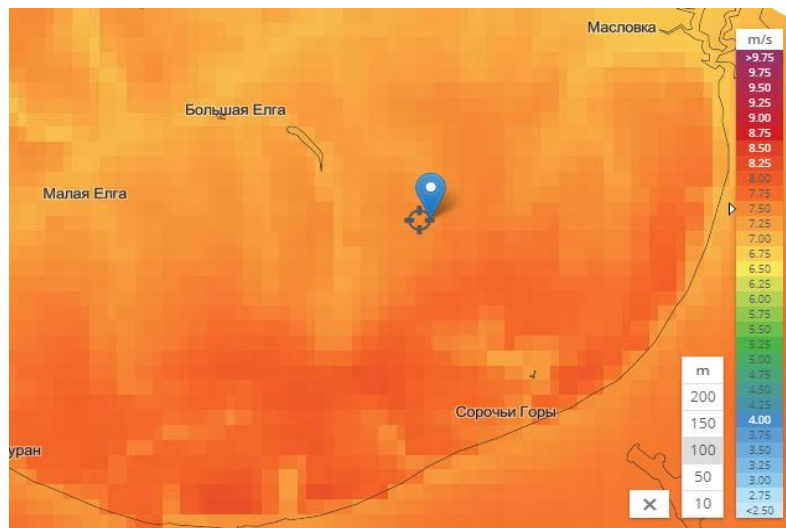


Figure 3. Map presenting the mean wind speed in Sorochi Gory

1.3. Grid Connection on the Site

On Sorochi Gory, there is an electrical substation connected to the grid of Tatarstan. Figures 4 and 5 show the grid over Tatarstan, in particular on Sorochi Gory [6].



Figure 4. Map presenting the grid over Tatarstan



Figure 5. Map presenting the grid over Sorochi Gory

The following figure shows the substation located in Sorochi Gory.

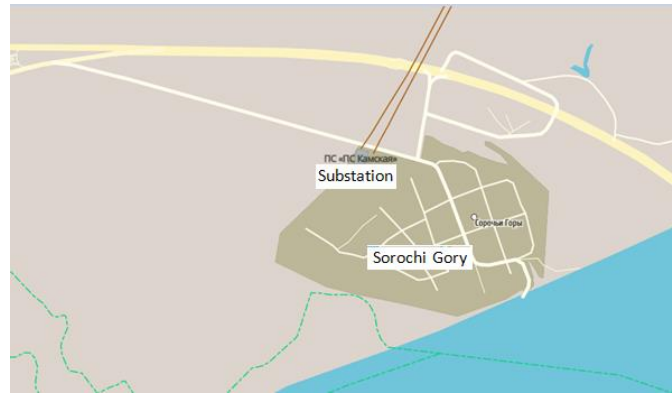


Figure 6. Map showing the substation in Sorochi Gory

A station nearby will reduce the cost of the cables, in addition batteries are not needed.

2. Panoramic View

2.1. Wind Farm Site Information

The following Figure 7 shows a view of dense forestry immediately northwest of the site.



Figure 7. Forestry in the northwest of the site

- Forestry extents have been obtained from aerial photography and site visit observations.
- The trees heights were estimated to be from approximately 9 m to 12 m.

As concluded the trees height is around 12m and no buildings exists, the grace is smoothly spread. To estimate the wind shear shown in the following equation can be used [7]:

$$\alpha = \frac{\ln(\frac{v_2}{v_1})}{\ln(\frac{h_2}{h_1})} \quad (1)$$

Where α is the wind shear, h_2 is the height at the top, h_1 is the height at the bottom, V_2 is the speed at the top and V_1 is the speed at the bottom [8]. On the other hand, when an overview of the site is available, the wind shear can be estimated according to the Table 1:

Table 1. The power law exponent α values according to the terrain description [9]

Terrain description	Power law exponent, α
Smooth, hard ground, lake or ocean	0.1
Short grass on untilld ground	0.14
Level country with foot-high grass, occasional tree	0.16
Tall row corps, hedges, a few trees	0.2
Many trees and occasional buildings	0.22-0.24
Wooded country-small towns and suburbs	0.28-0.3
Urban areas with tall buildings	0.4

From the Table 1, according to the description of the site, the wind shear can be estimated to be $\alpha=0.2$. As seen in the pictures of Figure 7, the biome around the mast is relatively smooth, that is why the shear factor α is relatively small which indicates that the wind is not fluctuating heavily [10].

2.2. Mast Information

The mast is set at point (431079, 6137641) with several sensors at several heights as seen in the Figure 8. In the following Figure 8, photographs looking west-southwest and south of the mast are presented.

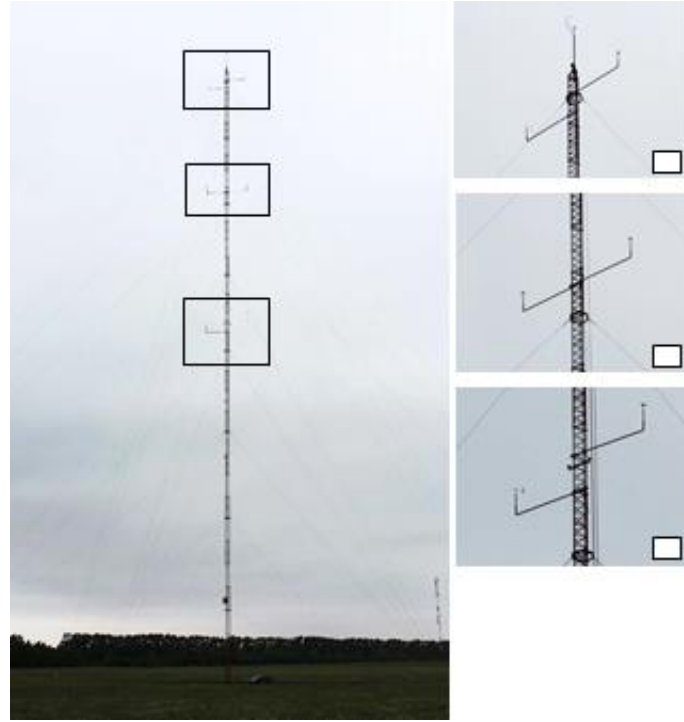


Figure 8. Photographs looking west-southwest and south of the mast

The sensors are set at different heights in order to measure the wind speed and wind direction at several tips. By using, the data of the anemometers in the shear Equation 1, the wind shear α can be precisely calculated. The wind shear Equation 1 should be filled by the proper data, where h_2 is the height of the higher anemometer 99 m, h_1 is the height of the lower one 94.3 m, V_2 is the speed at h_2 and V_1 is the speed at h_1 . Then this repeated for the anemometers at heights 72.6 m and 94.3 m [11]. The average wind shear is then calculated by averaging both the shears.

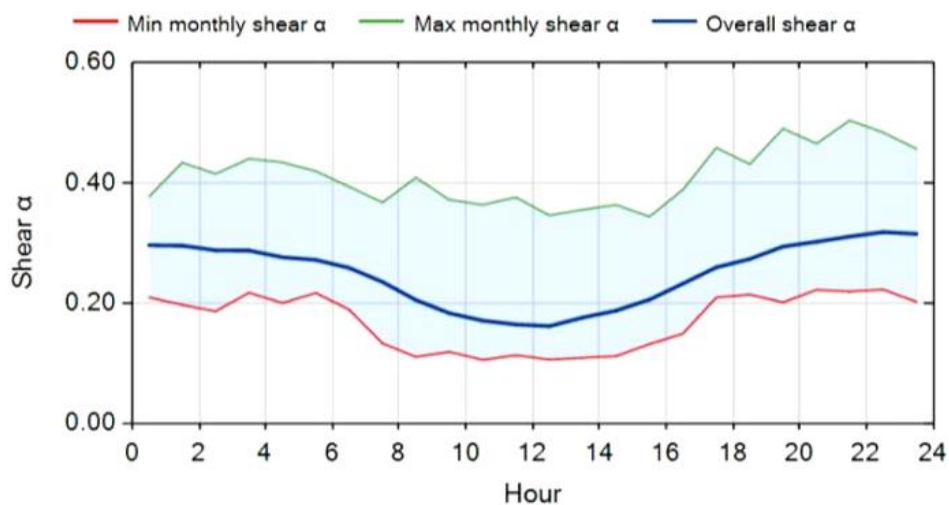


Figure 9. Maximum, minimum and average monthly wind shear

The blue line presents the average wind shear between the maximum α and the minimum α . The average is calculated to eliminate the uncertainty as much as possible.

3. Factors Affecting the Site

3.1. Site Access

Extreme ecological conditions can affect access to more remote sites, which can affect accessibility. A case of this may be a zone prone to serious snowdrifts during the winter season. The effect on energy will be subjected to the operations and maintenance plans [12].

3.2. Impact of Trees

Where obstacles to the flow (for example, trees in closeness to a pole or turbine) are present, it is crucial to consider the impact of these impediments on the wind flow model. The accompanying methodology has, therefore been adopted [13]. Zones of forestry and land cover have been examined, to build up both the area and tallness of trees.

- For every pole and turbine location, a viable decrease in the estimation or hub tallness is assessed, so as to represent the impact of trees as a snag to the wind flow. The determination of these statures depends on the displacement tallness of the trees, the vicinity of the pole or turbine to the trees, and the recurrence of the event of the relevant wind directions.
- Where suitable, a characteristic energy loss factor profile is determined, so as to represent any adjustments in the forestry (because of expected tree expansion or felling) during the initial ten years of the wind farm activity.
- For wind farm locations situated inside or near forestry or zones of trees, the effect of how the trees may change after some time and the impact that this will have on the wind flow over the site, and thus the energy production of the wind farm must be considered. The effect of future felling of trees, whenever known, may likewise need to be surveyed. This loss is normally determined on a site-explicit premise.

4. Turbines Limitations

4.1. Turbine Models

In the Table 2, the turbine models are present under consideration for the Sorochi Gory project [14].

Table 2. Proposed turbine model parameters

Turbine	Rated Power (MW)	Hub Height (m)	PC air density (Kg/m³)	Operational temperature range
Siemens Gamesa SG 3.4-132 3.465MW	3.465	97	1.24	-20 ⁰ C to +40 ⁰ C
Vestas V126-3.45 MW HTq	3.45	87	1.25	-20 ⁰ C to +45 ⁰ C
Lagerwey L100-2.5MW	2.52	99	1.225	-30 ⁰ C to +30 ⁰ C

4.2. Turbine Layouts

The wind farm format was structured with the aim of maximizing the energy output; a single wind farm design was intended for the Siemens Gamesa SG 3.4-132 3.465 MW turbine, as the biggest rotor diameter across the turbine model, the two other turbines models used the same layout for the analysis.

Computational optimization of the wind farm format has in this manner been embraced, utilizing DNV GL's WindFarmer Software. The accompanying limitations have been utilized for this optimization, for the Siemens Gamesa SG 3.4-132 3.465 MW turbine [15]:

- A 6.0 rotor diameter spacing between turbines in the prevailing wind directions;
- A 4.0 rotor diameter spacing between turbines in the non-prevailing wind directions;
- An elliptical constraint is used based on the above criteria;
- Terrain slope lower than 10°;
- A site boundary and presented in Figure 1.2;
- A setback distance of 300 m from the site boundary; and
- Further setback distances of:
 - 50 m from unpaved internal roads and 200 m from main roads;
 - 100 m from water areas;
 - 200 m from high voltage lines;
 - 300 m from forestry areas.

A map of the site showing the excluded zones and the allowed areas for placing wind turbines is presented in Figure 10.

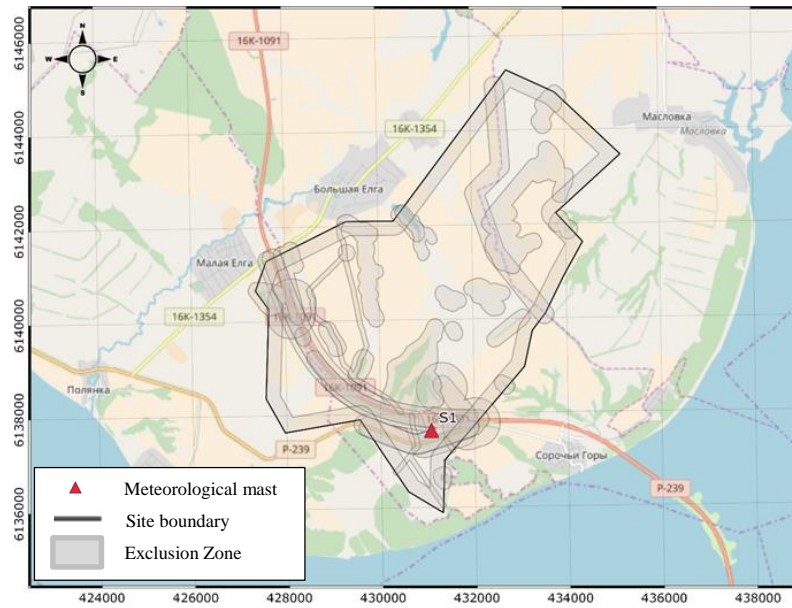


Figure 10. Excluded zones and allowed area for placing wind turbines at the Sorochi Gory Wind Farm site

5. Turbines Configurations

The following layout has been designed considering 60 turbine locations, with details given in Table 3 [16, 17].

Table 3. Turbine layout configurations

Configuration Id	Turbine type	Hub height (m)	Number of turbines	Rated power (MW)
1	Siemens Gamesa SG 3.4-132 3.465 MW	97	60	207.9
2	Vestas V126-3.45 MW HTq	87	60	207
3	Lagerwey L100-2.5 MW	99	60	150

The power delivered by a wind turbine is represented through its power curve, where a relation between the wind speed and the power generated is established. Each wind turbine has its own configuration which presents the power that can be produced at specified wind speeds, the availability of the turbines is assumed at 100% (no losses due to down time, icing, transformer losses, park effects etc.). The relationship between wind speed and power is defined by a power curve, which is unique to each turbine model.

Figures 11 to 13, illustrate the Siemens Gamesa SG3.4-132, 3.465MW, Vestas V126-3.45 HTq and Vestas V126-3.45 HTq wind turbine power curve respectively.

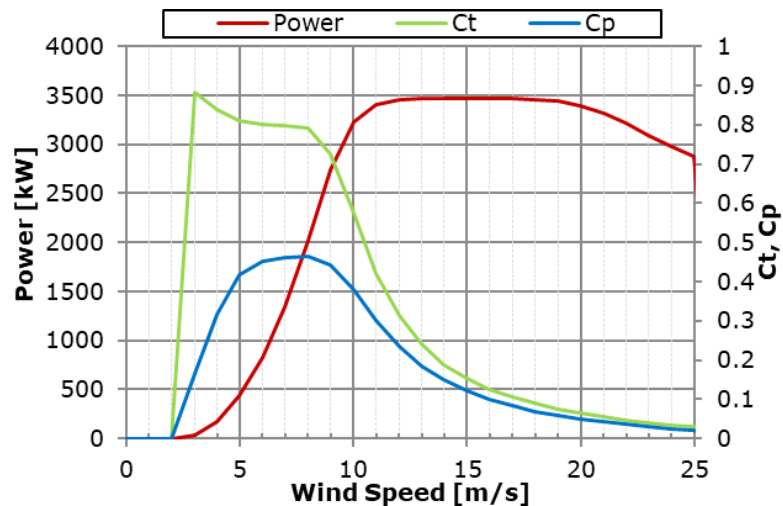


Figure 11. Power curve of the Siemens Gamesa SG3.4-132, 3.465MW turbine

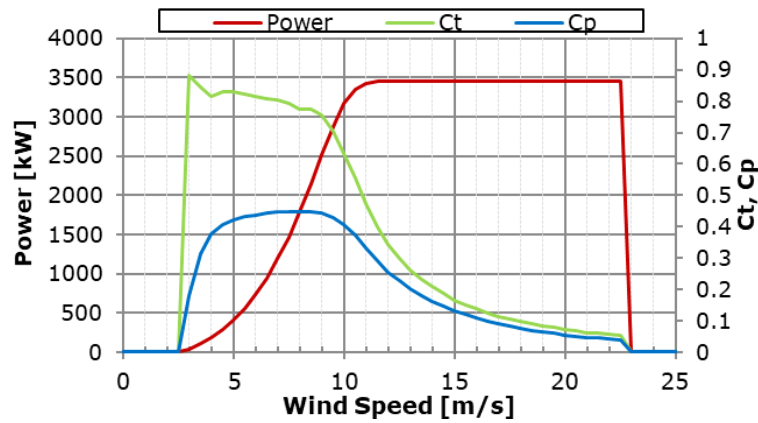


Figure 12. Power curve of the Vestas V126-3.45 HTq, turbine

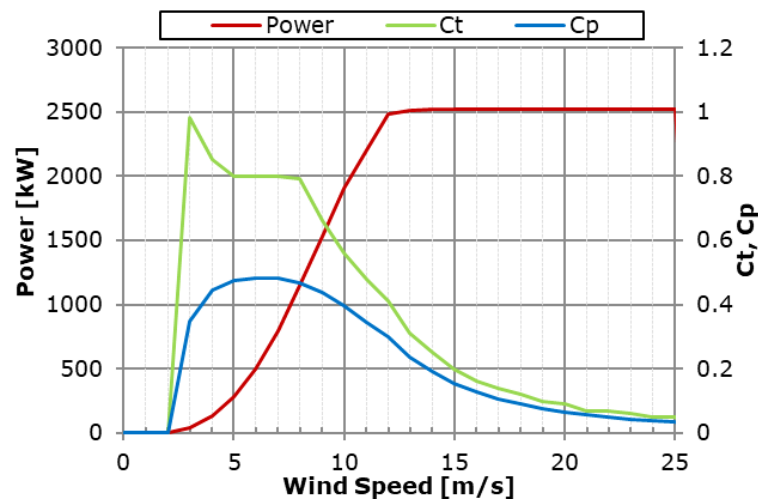


Figure 13. Power curve of the turbine Lagerwey L100-2.5 turbine

A map of the site showing the designed turbine layout and wind measurement location is presented in following Figure 14.

6. Capacity Factor

By using the capacity factor Equation (2), the most suitable turbine can be determined.

$$CF = \frac{E_{actual}}{E_{ideal}} \quad (2)$$

where E_{actual} is the real power generated by the turbine under specific data and the E_{ideal} is the maximum power that can be generated by the turbine.

The actual energy is calculated by multiplying the actual wind speed by the power referred to each speed. This power can be measured by using the power curve of each wind turbine. The ideal energy is calculated by multiplying the maximum wind speed reached by the rated power. The calculation is made for each proposed wind turbine.

Siemens Gamesa SG 3.4-132 3.465 MW

$$E_{actual} = 14,287,966.61$$

$$E_{ideal} = 30,353,330.70$$

Thus, the capacity factor is $CF = 47\%$

CF Vestas V126-3.45 HTq

$$E_{actual} = 13,507,385.38$$

$$E_{ideal} = 30,221,931.00$$

Thus, the capacity factor is $CF = 45\%$

CF Lagerwey L100-2.5 MW

$E_{\text{actual}} = 8,825,895.03$

$E_{\text{ideal}} = 30,353,330.70$

Thus, the capacity factor is $CF=29\%$

The capacity factor for all the proposed turbines is considered really good. The CF of the Lagerwey L100-2.5 MW has the lowest one, and Siemens Gamesa SG 3.4-132 3.465MW is the highest. However, from the economical perspective, a higher CF will cost much more on the turbine, and a lower one can be the most suitable as a higher capacity factor does not specifically mean that the wind farm investment vs. profit is higher, taking into consideration the price of the turbine.

7. Map of the Site

The following observations are made regarding the layout:

- It is noticed that ordinarily higher inter-turbines spacing ought to be applied. It was anyway required to decrease the inter-turbine separating to accomplish the highest wind farm capacity on the site while adjusting the requirement for lower wake losses and therefore lower potential fatigue loads.
- It is noticed that a primer examination of the structure proportionate turbulence intensities was led for the proposed turbines. Hence, it was chosen to receive the consequences of the optimization without any more changes or a decrease in turbine numbers. A portion of the turbine areas in the format is proposed in the prompt region of trees up to roughly 12 m in height. The height of these trees is significantly less than the proposed hub heights and the potential for elevated turbulence is small.

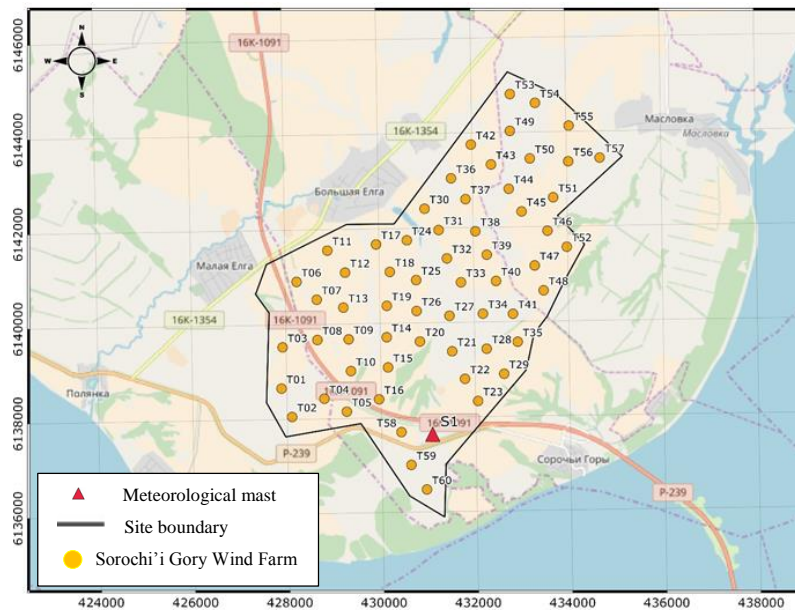


Figure 14. Map of the Sorochi Gory wind farm showing the mast location and the designed turbines layout

Table 4. Shows the terrain contour, roughness and forestry maps for the site

Site characteristic	Resulting input into analysis		Source
Terrain	11 Km radius digital terrain map with contours at 2.5 m intervals		Publicly available SRTM contour map.
Roughness	Roughness map with following categories:		Publicly available satellite imagery based on Davenport classification.
	Forested areas	0.5 m	
	Settlements	0.3 m	
	Light forestry	0.2 m	
	Bushes	0.15 m	
	Marshes	0.07 m	
	Site and surrounding areas	0.03 m	
	Water	0.0002 m	
Forestry	Forestry map of site area showing forestry of between 9 to 12 m in height		Publicly available satellite imagery

Table 4, displays the site characteristic.

8. Future Work

According to the presented data, the mast lies at a height of around 175 m, while the turbines' elevation shifts from roughly 85 to 175 m. The site pole position is, in this manner, considered not perfectly representative of turbines based at lower elevations, such as a group of turbines situated along the northern edge of the site. It is recommended to do additional measurements at the site, particularly in the northern part, which would serve to reduce these uncertainties. The uncertainty connected with horizontal flow modelling could also be further reduced by employing CFD (Computational Fluid Dynamics) [18].

An economical study should be conducted to estimate the optimal turbine configuration as the capacity factor is shown for each of them. Solar energy can be built around the turbines as the area is not suitable for residential use due to the noise made by the turbines; information about the site is given in Table 5 [19].

Table 5. Information regarding solar energy per year

Specific photovoltaic power output	Pvout	1129 kWh/kWp
Direct normal irradiation	DNI	1116 kWh/m ²
Global horizontal irradiation	GHI	1118 kWh/m ²
Diffuse horizontal irradiation	DIF	519 kWh/m ²
Global tilted irradiation at optimum angle	GTI	1336 kWh/m ²
Optimum tilt of PV modules	OPTA	39/180 °
Air temperature	TEMP	4.8 ° C
Terrain elevation	ELE	128 m

9. Conclusion

In this paper, the location of the project was presented. The wind speed and the grid's substation were found to be suitable for the project. For precise measures, a mast was built at the point (431079, 6137641); a panoramic view of the site including the mast were presented to estimate the wind shear α . Some of the factors that affect the site were examined, such as streets, water areas, high voltage lines, and forestry, in order to avoid the turbulence and wake as much as possible. The limitations of wind turbines were discussed and studied to calculate the spacing between them and estimate the locations for each of the wind turbines [20]. The capacity factor shows the different percentages for each of the turbines. Considering it with the price and the length of life of each turbine will lead to the estimation of the optimal wind turbine.

10. Declarations

10.1. Data Availability Statement

The data presented in this study are available in article.

10.2. Funding

The author received no financial support for the research, authorship, and/or publication of this article.

10.3. Institutional Review Board Statement

Not applicable.

10.4. Informed Consent Statement

Not applicable.

10.5. Declaration of Competing Interest

The author declares that there is no conflict of interests regarding the publication of this manuscript. In addition, the ethical issues, including plagiarism, informed consent, misconduct, data fabrication and/or falsification, double publication and/or submission, and redundancies have been completely observed by the author.

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